

## PEDCO Adsorptive Gas-Dryer Simulation Software

### Conservation Equations, Assumptions, Initial Conditions, Boundary Conditions, and Constitutive Relations

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#### PARTICLE CONSERVATION OF MASS (PARTICLE DIFFUSIVITY)

##### GOVERNING EQUATION

$$\frac{\partial q}{\partial t} + \varepsilon_p \frac{\partial c}{\partial t} = D_{eff} \frac{\partial}{\partial r} \left( \frac{\partial c}{\partial r} \right)$$

##### ASSUMPTIONS

- Gas phase storage term is negligible
- $D_{eff}$  is constant through particle
- $D_{eff}$  is independent of loading

##### INITIAL CONDITIONS

$$c(r, 0) = c_{initial}$$

$$q(r, 0) = q_{initial}$$

##### BOUNDARY CONDITIONS

$$\left( \frac{\partial c}{\partial r} \right)_{r=0} = 0$$

$$\left( D_{eff} \frac{\partial c}{\partial r} \right)_{r=R_s} = -K_f (c_B - c_R)$$

##### CONSTITUTIVE RELATIONS

- Desiccant Capacity

$$q = q(c, T)$$

- Mass Transfer Film Coefficient

*Sherwood Number*

$$Sh = \frac{2K_f R_s}{D_m} = 2.0 + 0.6 Re^{0.5} Sc^{0.33}$$

*Reynold Number*

$$Re = \frac{\rho_f V 2R_s}{\mu}$$

*Schmidt Number*

$$Sc = \frac{\mu}{\rho_f D_m}$$

- Ideal Gas Law

$$c = \frac{P_v}{R_v T}$$

- Effective Diffusivity

$$D_{eff} = \varepsilon_p D_p = \frac{\varepsilon_p D_m}{\tau}$$

where

$$D_m = D_{m,o} \left( \frac{P_o}{P} \right) \left( \frac{T}{T_o} \right)^{1.5}$$

## GAS STREAM CONSERVATION OF MASS

GOVERNING EQUATION

$$-\varepsilon D_L \frac{\partial^2 c}{\partial Z^2} + \frac{\partial}{\partial Z} (Vc) + \varepsilon \frac{\partial c}{\partial t} + (1 - \varepsilon) \frac{\partial \bar{q}}{\partial t} = 0$$

## ASSUMPTIONS

- Gas phase storage is neglected -  $\frac{\partial c}{\partial t} = 0$
- One dimensional – no gradients in radial direction
- Plug flow is assumed –  $D_L = 0$

## INITIAL CONDITIONS

$$c(Z, 0) = c_{initial}$$

$$\bar{q}(Z, 0) = \bar{q}_{initial}$$

## BOUNDARY CONDITIONS

$$c(0, t) = c_{inlet}$$

$$V(0, t) = V_{inlet}$$

## CONSTITUTIVE RELATIONS

- Superficial Velocity

$$V = \frac{Flow_{std} \sigma_{std}}{c_{gas} A_c}$$

- Gas Concentration

$$c_{gas} = \frac{(P_T - P_v)}{R_{gas} T}$$

- Average Loading

$$(1 - \varepsilon) \frac{\partial \bar{q}}{\partial t} = a k_f (c_b - c_R)$$

## GAS-ADSORBENT CONSERVATION OF ENERGY

## GOVERNING EQUATION

$$-\varepsilon K \frac{\partial^2 T_f}{\partial Z^2} + V \rho_f C_{p,f} \frac{\partial T_f}{\partial Z} + (1 - \varepsilon) \rho_s C_{p,s} \frac{\partial T_s}{\partial t}$$

$$= -(1 - \varepsilon) \Delta H \frac{\partial \bar{q}}{\partial t} - \frac{4h_v}{d_i} (T_f - T_v)$$

## ASSUMPTIONS

- Conduction heat transfer is neglected
- Energy storage term in gas phase is neglected
- Thermal equilibrium between fluid and solid is assumed, i.e.  $T_f(Z) = T_s(Z)$
- No radial temperature gradient in sorbent bed

## INITIAL CONDITIONS

$$T_f(Z, 0) = T_s(Z, 0) = T_{initial}$$

$$\bar{q}(Z, 0) = \bar{q}_{initial}$$

## BOUNDARY CONDITIONS

$$T(0, t) = T_{inlet}$$

$$V(0, t) = V_{inlet}$$

## CONSTITUTIVE RELATIONS

- Film heat transfer coefficient to vessel

*Nusselt Number*

$$Nu = \frac{2h_v R_s}{K_f} = 2.0 + 0.369 Re^{0.64} Pr^{0.33}$$

*Reynold Number*

$$Re = \frac{\rho_f V 2R_s}{\mu}$$

*Prantl Number*

$$Pr = \frac{C_{p,f} \mu}{K_f}$$

## VESSEL CONSERVATION OF ENERGY

### GOVERNING EQUATION

$$\pi d_i h_v (T - T_v) = \frac{\pi}{4} (d_o^2 - d_i^2) \rho_v C_v \frac{\partial T_v}{\partial t} + \frac{\pi d_o}{R_a} (T_v - T_{amb})$$

### ASSUMPTIONS

- No radial temperature gradient through vessel
- No axial conduction through vessel

### INITIAL CONDITIONS

$$T_v(Z, 0) = T_{v,initial}$$

### BOUNDARY CONDITIONS

$$T_{amb}(t) = T_{amb}$$

### CONSTITUTIVE RELATIONS – none

## GAS CONSERVATION OF MOMENTUM

### GOVERNING EQUATION

$$\frac{\partial P}{\partial Z} = f \left( \frac{\sigma V^2}{2R_s} \right)$$

### ASSUMPTIONS – none

### INITIAL CONDITIONS – none

### BOUNDARY CONDITIONS

$$P(0, t) = P_{inlet}$$

### CONSTITUTIVE RELATION

- Ergun friction factor

$$f = \left( \frac{1 - \varepsilon}{\varepsilon^3} \right) \left[ \frac{150(1 - \varepsilon)}{\text{Re}} + 1.75 \right]$$

## NOMENCLATURE

- $a$  – sorbent external surface area [ $\text{ft}^2/\text{ft}^3$ ]
- $A_c$  – Bed cross sectional area [ $\text{ft}^2$ ]
- $c$  – gas phase concentration [ $\text{lb}_{\text{H}_2\text{O}}/\text{ft}^3_{\text{g}}$ ]
- $c_B$  – gas phase concentration in bulk stream [ $\text{lb}_{\text{H}_2\text{O}}/\text{ft}^3_{\text{g}}$ ]
- $c_{\text{gas}}$  – concentration of gas (density) [ $\text{lb}/\text{ft}^3$ ]
- $c_{\text{initial}}$  – initial gas phase concentration [ $\text{lb}_{\text{H}_2\text{O}}/\text{ft}^3_{\text{g}}$ ]
- $c_{\text{inlet}}$  – gas phase concentration at bed inlet [ $\text{lb}_{\text{H}_2\text{O}}/\text{ft}^3_{\text{g}}$ ]
- $C_{P,f}$  – fluid specific heat [Btu/lb-R]
- $C_{P,s}$  – sorbent specific heat [Btu/lb-R]
- $C_v$  – vessel specific heat [Btu/lb-R]
- $c_R$  – gas phase concentration at sorbent particle surface [ $\text{lb}_{\text{H}_2\text{O}}/\text{ft}^3_{\text{g}}$ ]
- $D_{\text{eff}}$  – effective diffusivity through adsorbent particle [ $\text{ft}^2/\text{min}$ ]
- $d_i$  – vessel inside diameter [ft]
- $D_L$  – axial dispersion coefficient – [ $\text{ft}^2/\text{min}$ ]
- $D_m$  – molecular diffusivity [ $\text{ft}^2/\text{min}$ ]
- $D_{m,o}$  – molecular diffusivity at standard temperature and pressure [ $\text{ft}^2/\text{min}$ ]
- $d_o$  – vessel outside diameter [ft]
- $D_p$  – sorbate pore diffusivity [ $\text{ft}^2/\text{min}$ ]
- $Flow_{\text{std}}$  – flow referenced to standard temperature and pressure [scfm]
- $K$  – thermal conductivity of sorbent bed [Btu/min-ft-R]
- $K_f$  – external fluid film mass transfer coefficient [ft/min]
- $h_v$  – film coefficient to vessel [Btu/min-ft<sup>2</sup>-R]
- $P$  – pressure [ $\text{lb}_f/\text{ft}^2$ ]
- $P_{\text{inlet}}$  – pressure at bed inlet [ $\text{lb}_f/\text{ft}^2$ ]
- $P_o$  – standard pressure [ $\text{lb}_f/\text{ft}^2$ ]
- $P_T$  – total gas pressure [ $\text{lb}_f/\text{ft}^2$ ]
- $P_v$  – sorbate vapor pressure [ $\text{lb}_f/\text{ft}^2$ ]
- $\underline{q}$  – solid phase concentration [ $\text{lb}_{\text{H}_2\text{O}}/\text{ft}^3_{\text{s}}$ ]
- $\bar{q}$  – average solid phase concentration [ $\text{lb}_{\text{H}_2\text{O}}/\text{ft}^3_{\text{s}}$ ]
- $\underline{q}_{\text{initial}}$  – initial solid phase concentration [ $\text{lb}_{\text{H}_2\text{O}}/\text{ft}^3_{\text{s}}$ ]
- $\bar{q}_{\text{initial}}$  – average initial solid phase concentration [ $\text{lb}_{\text{H}_2\text{O}}/\text{ft}^3_{\text{s}}$ ]
- $r$  – radial coordinate for adsorbent [ft]
- $R_a$  – resistance to ambient heat loss from vessel [min-ft<sup>2</sup>-R/Btu]
- $R_{\text{gas}}$  – gas constant of bulk gas [ft-lb<sub>f</sub>/lb<sub>m</sub>-R]
- $R_s$  – adsorbent particle radius [ft]
- $R_v$  – gas constant of sorbate [ft-lb<sub>f</sub>/lb<sub>m</sub>-R]
- $t$  – time [min]
- $T$  – temperature [R]
- $T_{\text{amb}}$  – ambient temperature [R]
- $T_f$  – fluid temperature [R]
- $T_{\text{inlet}}$  – temperature of inlet fluid [R]

- $T_o$  – standard temperature [R]
- $T_s$  – sorbent temperature [R]
- $T_v$  – vessel temperature [R]
- $T_{v,initial}$  – initial vessel temperature [R]
- $V$  – superficial velocity [ft/min]
- $V_{inlet}$  – superficial velocity at bed inlet [ft/min]
- $Z$  – axial coordinate [ft]
- $\Delta H$  – heat of adsorption [Btu/lb]
- $\varepsilon$  - voidage of sorbent bed [ft<sup>3</sup>/ft<sup>3</sup>]
- $\varepsilon_p$  – porosity of adsorbent particle [ft<sup>3</sup>/ft<sup>3</sup>]
- $\rho_f$  – fluid density [lb/ft<sup>3</sup>]
- $\rho_s$  – sorbent density [lb/ft<sup>3</sup>]
- $\rho_{std}$  – fluid density at standard pressure and temperature [lb/scf]
- $\rho_v$  – vessel density [lb/ft<sup>3</sup>]
- $\tau$  - tortuosity [ft/ft]
- $\mu$  - viscosity [lb<sub>m</sub>/ft-min]