P E D C O Process & Equipment Development Corporation

Adsorptive Gas-Dryer Software

PEDCO's Adsorptive Gas-Dryer Simulation software predicts the performance of adsorptive desiccant dryers. The Desiccant Dryer Engineer specifies the dryer type, dryer geometry, desiccant type, operating conditions, and ambient conditions. The program simulates the dryer performance by solving the transient conservation equations of mass, energy, and momentum for the specified system. Output includes dew point, desiccant loading, temperature, etc. as a function of time and bed position. PEDCO's Adsorptive Gas-Dryer Simulation is intended for:

- manufacturers of desiccant and desiccant dryers
- engineering companies specifying and evaluating desiccant dryers
- compressed air system auditors optimizing performance of desiccant dryers
- end users comparing, evaluating, and selecting desiccant dryers
- system engineers using desiccant dryers as an integral part of the system
- service personnel troubleshooting desiccant dryer performance, etc.

DRYER TYPES

GASES

The software can be used to simulate performance of:



Thermal Swing (Heated) Dryers

- Atmospheric Pressure Blower Purge
- Closed Loop Blower Purge
- Heated Purge
- Heat of Compression

Pressure Swing (Heatless) Dryers

- Conventional
- Vacuum Assisted
- Single Tower
- Once Through Dryers (Non-regenerative)

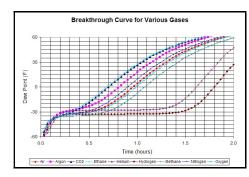
The Dryer Engineer can select from a total of 146 different dryer configurations.



Drying of:

- Argon
- Carbon Dioxide
- Ethane
- Helium
- Hydrogen
- Methane
- Nitrogen
- Oxygen
- Mixture of above gases

can be simulated. Based on the dryer type, the gas being dried and gas used to regenerate the desiccant can be different.



DESICCANTS

The program contains isotherms and property data for all the typical desiccants:

- Activated Alumina
- 3A, 4A, and 13X Molecular Sieves
- Granular and Spherical Silica Gels
- User specified desiccants

Any desiccant diameter can be specified. Aging factors can be specified to study the impact of desiccant aging and contamination on dryer performance.

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		Desio	oant				
	Drying Inter Layer 1	Lager 2		Layer2		Dising Date Layer II	
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Up to four layers of desiccant can be specified based on desiccant type, desiccant diameter, or aging factor. Within each layer a mixture of up to four desiccants can be specified.

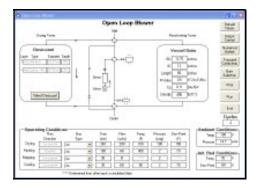
APPLICATIONS

Uses for the program are unlimited for the Desiccant Dryer Engineer. Just a few examples of its use include:

- · Predict performance of an existing dryer operating at off-design conditions
- Assist in development of an energy management system
- Enable a better understanding of the inner workings of a desiccant dryer to optimize performance and design
- · Evaluate reactivation scheme options to intelligently conduct a cost-benefit analysis
- Conduct a sensitivity analysis to determine purge air requirements for a pressure swing dryer as a function of required dew point, inlet temperature, inlet pressure, inlet relative humidity, desiccant type, desiccant diameter, etc.
- Study the effects of desiccant particle size on dryer performance
- Study the effect of desiccant layering on drying and reactivation performance
- Develop new energy efficient dryers
- Create support documents for proposal presentation

INPUT

The Engineer enters input data describing the dryer and operating conditions in English or SI units into intuitively designed input forms.



Every form includes a *Default Button* that can be clicked to populate all fields with a set of *Default Data*.

Alternatively, a data file generated during a previous simulation run can be specified and data from that run will be read into the input forms. Any desired changes from the previous run can then be made.

Desiccant properties, transport coefficients, numerical system specifications, output control parameters, etc can be provided by the Engineer - or the programs defaults can be selected.

Four levels of input data checking are included to assure a valid data set is provided. If a data value is deemed unusual, a *warning* is issued that the Engineer can ignore. If a data input *error* is detected, a change must be made before continuing.

- 1. Individual values are checked as entered and low and high warnings and errors are issued as appropriate.
- 2. Upon exiting an input data form, all data fields are checked to assure a complete set of data is provided.
- Prior to running the simulation, all data forms are checked to assure they have been completed. If not, the program prompts the operator to enter data or use the programs default values.
- 4. When the program begins, relationships between data are checked. For example, the program checks to see if desiccant fluidization is a potential problem.

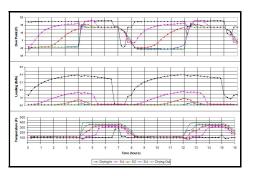
OUTPUT

Simulated data is output to an Excel® spreadsheet workbook. All input conditions and simulated output data are saved in one workbook. The program creates a *Model Number* type name for the workbook capturing much of the specific information regarding the dryer and operating conditions.

	A	B	С	D	E	F	G	н	1	J	K.	L
1	Date	12/3/2003				Open Loop	Blower					
2	Stat Time											
3	End Time	6:12 PM		Desiccare.					Vessel Da	6a		
4			Draing Inlet			Draing Outlet						
8			Lager 1	Lager 2	Lager 3	Lager 4		00	12.75	inches		
8		Tgpe	Act Alumina	None	None	None		D	12	inches		
7	0	Diameter (inches)	0.125					Length	60	inches		
		Depth (%)	100					B-Value	0.5	R*2-kt-F/E	tu	
		Shape Factor	1					Co	0.11	Btufb-F		
10		13% Aging Factor	0					Density	490	Ible'3		
11)	01% Aging Factor	0									
12		Tortuositu	2.7								2	Celle
13												1
14				Operatin	og Conditions					Am	bient Cond	tions
15		Flow	Gas	Time	Flow	Temp.		Dev Point		Тепр	100	F
16		Direction	Type	(min)	(sofm)	(F)	(psig)	(F)		Pressure	14.7	psia
17	Drying	Co-current	Air	240	200	100	100	100				
13	Heating	Counter	Ait	193	60	400	2	70				
19	Stripping	Co-outlent	Ait	30	8		2				Bed Conc	
20	Cooling	Co-outrent	Air	30	60	80	2	70		Тепр	70	F
21										Dew Point	-60	F
22												
23		Output Control			Numerical State	m						
24												
25	Output det	alled data every			Bed Grids	120						
28	1	cucles.			Bead Shells	3						
27	60	min. during coole,	and		Time Step	1						
28	6	inches thrubed.										
23	Output alo	data everu						Transport 0	Coefficien	ls.		
33	1	cycles and										
31	15	minuter,				Gas-to-Vessel F	leat Transfe	r Coellicient				
32	Output ma	terial and energy ba	lance overs							0.64	0.33	
33	1	cycles and				Nu r	2		0.369	Re	Pr	
34	240	minutes during ca	sle.									
35		p. and cone, distrib				Gas-to-Desicca	nt Mass Tr.	insier Coelli	lient.			
36	1	cucles								0.5	0.33	
37	Plot Outpu	t Data Continuous	N	Yes		Sha	2		0.6	Re	Sc	
22	Cutrue Ber	ation Counter		No								

Output data includes:

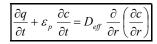
- Dryer outlet Dew Point and Temperature as a function of Time
- Desiccant Bed Temperature, Loading, and Dew Point distributions as a function of Time (output in tabular and plotted formats)
- Water Loading Distribution in a Desiccant Particle as a function of Bed Position and Time
- Desiccant and Gas Properties
- Transport Coefficients Gas-to-Vessel Heat Transfer Coefficient, Gas-to-Desiccant Mass Transfer Coefficient, Desiccant Bead Effective Diffusivity, etc.



The capabilities of Excel® can be utilized to manipulate and plot data in a format most suitable for the objectives of the immediate project.

SOLUTION ALGORITHM

The program solves the system of nonlinear partial-differential equations of mass, momentum, and energy describing the physics of adsorption.



Constitutive relations such as the ideal gas law, desiccant isotherms, correlations for molecular diffusivity in a desiccant particle, etc are utilized. The system of differential equations is solved using a finite-difference technique by dividing the bed into a finite number of thin pancake sections and a representative desiccant bead in each pancake into a finite number of shells.

Public Function CoPresoProp(L As Double, Void As Double, Ro As Double, Co U As Double, Vis As Double, Shape=factor As Double) As Double Function to calculate pressure drop (hrough a packed bed Reference - Principles of Asorption by Ruthwen, page 206 'CoPresoProp - column pressure drop [lb_fft*2] 'L - bed length [[t] 'R - sortent pielet radius [th] 'S hapeFactor - shape factor to account for non spherical geometries [dimensionless] 'U - supeficial ges veicch; [fmin] 'Vis - gas viscosity [lb/mtmi] 'Vid - voidage of packed bed [dimensionless] 'Declare variable types DIm Re As Double; FA Bouble 'Reynolds number Re = Den 'U 2' Rp / Vis 'Friction factor F = (1 - Void) / Vid 4 '3) * (150 * (1 - Void) / Re + 1.75) 'Pressure drop CoIPresDrop = F * L / (2 * Rp) * (U / 60) * 2 * Den / 32.2 * ShapeFactor End Function	
Reference - Principles of Adsorption by Ruthvén, page 206 ColPresofro- column pressure drop [b_f/th*2] Den - gas density [lo_m/th*3] L - beal length [ft] 'Rp - sotherit pellet radius [ft] 'ShapeFactor - shape factor to account for non spherical geometries [dimensionless] 'U - superficial gas velocity [ft/min] 'Void - voldage of packed bed [dimensionless] 'Declare variable types Dm Re As Double, F.As Double Reynolds number Re = Den 'U 2 * Rp /Vis 'Friction factor F = ((1 - Void) / Void * 3)* (150 * (1 - Void) / Re + 1.75) 'Pressure drop ColPresDrop = F * L / (2 * Rp) * (U / 60) * 2 * Den / 32.2 * ShapeFactor	Public Function ColPresDrop(L As Double, Void As Double, Rp As Double, Den As Double, _ U As Double, Vis As Double, ShapeFactor As Double) As Double
Reference - Principles of Adsorption by Ruthvén, page 206 CollPrestOre - column pressure drop [b_fth*2] Den - gas density [lb_mth*3] L - beal length [tt] 'Rp - sothert pellet radius [tt] 'ShapeFactor - shape factor to account for non spherical geometries [dimensionless] U - superficial gas velocity [thtmin] 'Void - voldage of packed bed [dimensionless] 'Declare variable types Dm Re As Double, FAs Double Reynolds number Re = Den 'U 2 * Rp /Vis 'Friction factor F = ((1 - Void) / Void * 3)* (150 * (1 - Void) / Re + 1.75) 'Pressure drop CollPresDrop = F * L / (2 * Rp)* (U / 60)* 2 * Den / 32.2 * ShapeFactor	' Function to calculate pressure drop through a packed bed
 CollPresDrop - column pressure drop [ib_fft*2] Den - gas density [ib_mft*3] L - bed length [ft] Rp - sortent pielet radius [ft] ShapeFactor - shape factor to account for non spherical geometries [dimensionless] U - superficial ges velocity [ftm/m] Yold - voldage of packed bed [dimensionless] Declare variable types Dim Re As Double F. As Double Reymolds number Re - Don ' 2 * 2 R / Vis Friction factor F = (1 - Void) / Viod ' 3)* (150 * (1 - Void) / Re + 1.75) Pressure drop F L / (2 * Rp)* (U / 60)* 2 * Den / 32.2 * ShapeFactor 	
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¹ L - bed length [t] ⁻ ¹ R ₂ - sothert belief radius [t] ¹ ShapePactor - shape factor to account for non spherical geometries [dimensionless] ¹ Us - gas viscosity [lib/tmin] ¹ Vis - gas viscosity [lib/tmin] ¹ Vida - voldage of packed bed [dimensionless] ¹ Declarer variable types Dim Re A 50 Double FA 50 Double ¹ Reymodis number Re - Den ' U 2' Re / Vis ¹ Friction factor F = (1 - Vold) / Vold * 3) * (150 * (1 - Vold) / Re + 1.75) ¹ Pressure drop CollPresDrop = F ¹ L / (2 * Rp) * (U / 60) * 2 * Den / 32.2 * ShapeFactor	
 Rp - sorberit pellet radius [ft] ShapeFactor - shape factor to account for non spherical geometries [dimensionless] J - superficial gas velocity [ft/min] Void - voidage of packed bed [dimensionless] Declare variable types Dim Re A 5 Double ; RA 5 Double Reynolds number Re = Den 'U 2 * Rp /Vis Friction factor F = (1 + Void) / Void * 3)* (150 * (1 - Void) / Re + 1.75) Persure drop p = F 'L /(2 * Rp) * (U / 60) * 2 * Den / 32.2 * ShapeFactor 	
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* Vis - gas viscosity [lib/tm/m] * Void - voidage of packed bed [dimensionless] * Declare variable types Dim Re A soluble, FAS Double Reynolds number Re ⊃ Den 'U *2 * Rp / Vis * Friction factor F = (01 - Void) / Void * 3) * (150 * (1 - Void) / Re + 1.75) * Pressure drop ColPresDrop = F * L / (2 * Rp) * (U / 60) * 2 * Den / 32.2 * ShapeFactor	
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ColPresDrop = F * L / (2 * Rp) * (U / 60) * 2 * Den / 32.2 * ShapeFactor	
End Function	
	End Function

The system of non-linear algebraic equations created by discretizing the differential equations is solved using the Newton-Raphson method.

PRICING

Perpetual License

- Complete Program \$13,500 U.S.
- Pressure Swing (Heatless) Only \$7,000 U.S.
- Thermal Swing (Heated) Only \$7,000 U.S.

Training

• \$1,500 U.S. / day plus travel expenses

Process & Equipment Development Corporation

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